

Amendments to the Claims:

The listing of claims will replace all prior versions, and listings, of claims in the application:

Listing of Claims:

Claim 1. (Currently Amended) A method for reducing bias error in a Vibrating Structure Gyroscope having a vibrating structure, primary drive means for putting the vibrating structure into carrier mode resonance, primary pick-off means for sensing carrier mode motion, secondary pick-off means for sensing response mode vibration of the vibrating structure in response to applied rotation rate, secondary drive means for applying a force to control the response mode motion, closed loop primary control loops for maintaining a fixed amplitude of motion at the primary pick-off means and for maintaining the drive frequency at the resonance maximum, and secondary control loops and for maintaining a null at the secondary pick-off means, in which the ratio SF_{QUAD} divided by $SF_{IN-PHASE}$ is measured from the secondary control loop to provide a direct measurement of $\sin(\phi_{SD} + \phi_{PPO})$, according to the relationship;

$$SF_{QUAD} = SF_{IN-PHASE} \times \sin(\phi_{SD} + \phi_{PPO})$$

where SF_{QUAD} is the quadrature scalefactor, $SF_{IN-PHASE}$ is the in-phase scalefactor, ϕ_{SD} is the phase error in the secondary drive means and ϕ_{PPO} is the

phase error in the primary pick-off means, the total phase error ϕ_E is obtained directly from the measured Sin ($\phi_{SD} + \phi_{PPO}$) according to the relationship;

$$\phi_E = \phi_{SD} + \phi_{PPO}$$

and phase corrections are applied to one of the secondary drive means ~~and/or~~ and the primary pick-off means to reduce the phase error ϕ_E and hence the quadrature bias error to enhance the performance of the gyroscope.

Claim 2. (Original) A method according to Claim 1, when used with a gyroscope having a silicon vibrating structure.

Claim 3. (Original) A method according to Claim 2, when used with a gyroscope having a substantially planar, substantially ring shaped vibrating structure.

Claim 4. (Previously Presented) A method according to Claim 1, when used with a gyroscope having analogue primary and secondary control loops with variable value capacitors, in which the phase corrections are applied by varying the values of the variable value capacitors in the secondary control loop relating to the secondary drive means and/or the values of the variable value capacitors in the primary control loop relating to the primary pick-off means to adjust ϕ_{SD} and/or ϕ_{PPO} such that ϕ_E is minimised in value.

Claim 5. (Previously Presented) A method according to Claim 1, when used with a gyroscope having digital primary and secondary control loops, in which the phase corrections equal to ϕ_E are applied to the secondary drive means

via the secondary control loop in a manner such as to cross-couple in-phase and quadrature drive channels by an amount equal and opposite to the combined effect of the phase errors in the vibrating structure control system.

Claim 6. (Previously Presented) A method according to Claim 1, when used with a gyroscope having digital primary and secondary control loops, in which the phase corrections equal to ϕ_E are applied to the primary pick-off means by the primary control loop in a manner such as to cross-couple in-phase and quadrature drive channels by an amount equal and opposite to the combined effect of the phase errors in the vibrating structure control system.

Claim 7. (Previously Presented) A method according to Claim 4, in which in-phase and quadrature signal components are each multiplied by $\sin \phi_{\text{CORR}}$ and $\cos \phi_{\text{CORR}}$, where ϕ_{CORR} is the phase correction, and the effective phase of each in-phase and quadrature channel adjusted according to the summations.

$$\text{Quadrature}_{\text{CORR}} = \text{Quadrature} \times \cos \phi_{\text{CORR}} + \text{In-phase} \times \sin \phi_{\text{CORR}}$$

and

$$\text{In-phase}_{\text{CORR}} = \text{In-phase} \times \cos \phi_{\text{CORR}} - \text{Quadrature} \times \sin \phi_{\text{CORR}}.$$

Claim 8. (Original) A method according to Claim 6, in which ϕ_{CORR} is adjusted in accordance with operating temperature of the gyroscope to maintain ϕ_E at a minimised value.

Claim 9. (Cancelled)

Claim 10. (Currently Amended) A Vibrating Structure Gyroscope ~~operated according to the method of Claim 1.~~ having a vibrating structure, primary drive means for putting the vibrating structure into carrier mode resonance, primary pick-off means for sensing carrier mode motion, secondary pick-off means for sensing response mode vibration of the vibrating structure in response to applied rotation rate, secondary drive means for applying a force to control the response mode motion, closed loop primary control loops for maintaining a fixed amplitude of motion at the primary pick-off means and for maintaining the drive frequency at the resonance maximum, and secondary control loops and for maintaining a null at the secondary pick-off means, in which the ratio SF_{QUAD} divided by $SF_{IN-PHASE}$ is measured from the secondary control loop to provide a direct measurement of $\sin(\phi_{SD} + \phi_{PPO})$, according to the relationship:

$$SF_{QUAD} = SF_{IN-PHASE} \times \sin(\phi_{SD} + \phi_{PPO})$$

where SF_{QUAD} is the quadrature scalefactor, $SF_{IN-PHASE}$ is the in-phase scalefactor, ϕ_{SD} is the phase error in the secondary drive means and ϕ_{PPO} is the phase error in the primary pick-off means, the total phase error ϕ_E is obtained directly from the measured $\sin(\phi_{SD} + \phi_{PPO})$ according to the relationship:

$$\phi_E = \phi_{SD} + \phi_{PPO}$$

and phase corrections are applied to one of the secondary drive means and the primary pick-off means to reduce the phase error ϕ_E and hence the quadrature bias error to enhance the performance of the gyroscope.